

## CONTROLLABLE PHOTOPOTENTIOMETRIC OPTOCOUPLEDERS

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*Photopotentiometric optocouplers (PPO) are electronic equivalents of mechanical resistor potentiometers. With PPOs the output quality is resistance (voltage or current) and it is converted into a function by the LED current rather than by the rotation angle of the potentiometer axle*

**Keywords:** Optocouplers, Photopotenciometer, Control, LED

### 1. INTRODUCTION

The law for changing the potentiometer resistance by means of the rotation angle can be linear, logarithmic and antilogarithmic.

PPOs can be designed with one or two optocouplers.

### 2. CIRCUITS OF PHOTOPOTENTIOMETRIC OPTOCOUPLEDERS

The simplest PPO circuit with a photodiode optocoupler is shown in fig. 1.

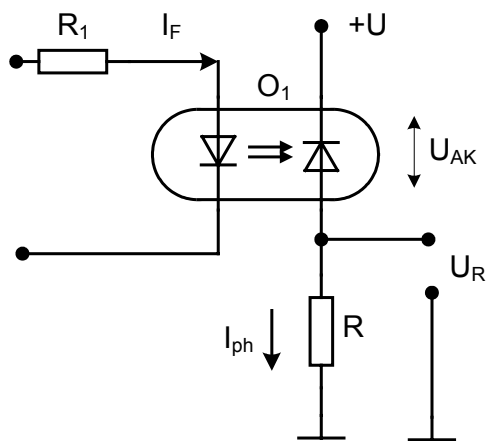


Fig. 1

The photodiode of the optocoupler  $O_1$  and the resistor  $R$  form a controllable voltage divider.

The photocurrent in the output circuit is:

$$(1) I_{ph} = CTR \cdot I_F$$

The output voltage is: ( $I_D \ll I_{ph}$ )

$$(2) U_R = I_{ph} \cdot R = CTR \cdot I_F \cdot R = \text{const. } I_F$$

$$(3) U = U_{AK} + U_R$$

Let  $U = 12 \text{ V}$ ,  $CTR = 10\%$ ,  $R = 10 \text{ k}\Omega$

when  $I_F = 1 \text{ mA}$ ,  $I_{ph} = 100 \mu\text{A}$ ,  $U_R = 1 \text{ V}$

$I_F = 10 \text{ mA}$ ,  $I_{ph} = 1 \text{ mA}$ ,  $U_R = 10 \text{ V}$

The change range of the output voltage is:

$$(4) D = 10/1 = 10$$

A greater change range of the output voltage can be obtained when an operational

amplifier is used - fig. 2.

$$(5) \quad U_o = -U_I \cdot \frac{R_F}{R_{ph}(I_F)}$$

For example, when  $I_F = 20 \text{ mA}$   $R_{ph} = 100 \Omega$

$I_F = 0 \text{ mA}$   $R_{ph} = 100 \text{ M}\Omega$  и  $R_F = 100 \text{ M}\Omega$

The range:

$$(6) \quad D = \frac{100 \text{ M}\Omega}{100 \Omega} = 10^6$$

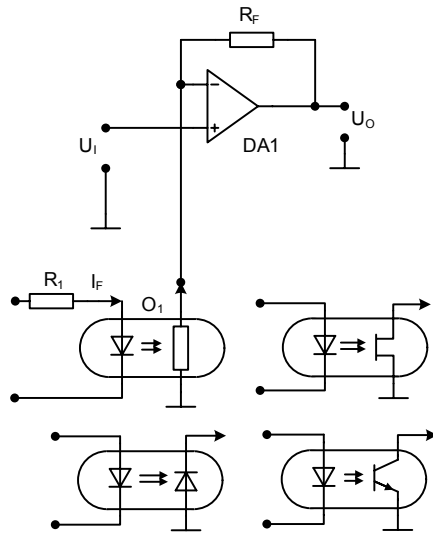


Fig.2

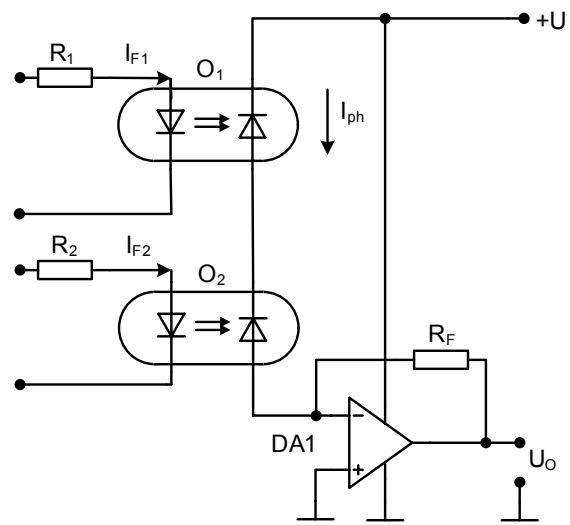


Fig. 3

For a linear change of the PPO output voltage by the LED current -  $I_F$  a transimpedance amplifier (DA1) current-voltage should be used – fig. 3.

$$(7) \quad U_o = - I_{ph} \cdot R_F$$

$$(8) \quad U_o = CTR_2 \cdot I_{F2} \cdot R_F$$

Let  $CTR = 10 \%$ ,  $R_F = 1 \text{ M}\Omega$ ,  $I_{ph} = 5 \mu\text{A}$ ,  $U_o = - 5 \cdot 10^{-6} \cdot 1 \cdot 10^6 = 5 \text{ V}$

PPOs are suitable for operating with low LED currents up to 1 mA.

### 3. CIRCUITS OF STEREPHOTOPOTENTIOMETRIC OPTOCOUPLEDERS

In order to obtain a stereopotentiometer, PPOs must have two channels – fig. 4.

$$(9) \quad U_{O1}, U_{O2} = f(I_F)$$

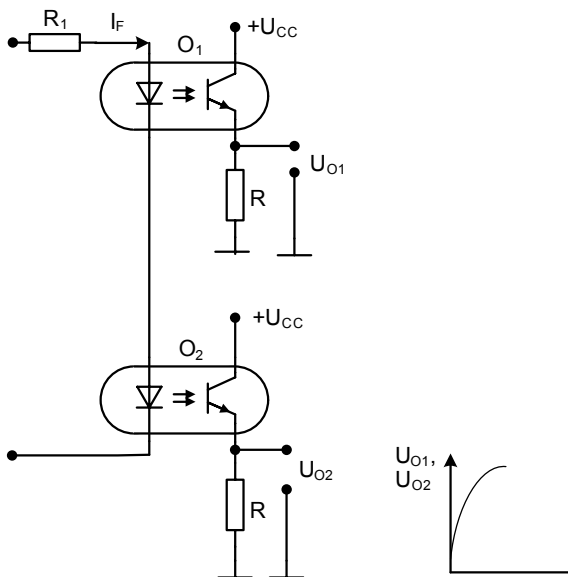


Fig. 4

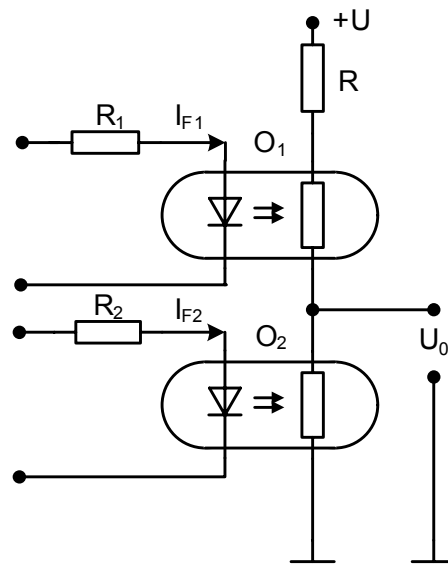


Fig. 5

#### 4. PHOTOPOTENTIOMETRIC OPTOCOUPLEDERS WITH DYNAMIC LOAD

The law for changing the output voltage by the current  $I_F$  is logarithmic.

PPOs are built with two basic optocoupler types:

- Photoresistor optocouplers (PRO) – fig. 5
- Photodiode optocouplers (PDO) – fig. 6
- Phototransistor optocouplers (PTO) – fig. 7
- Darlington phototransistor optocouplers (DFTO) – fig.8
- Optocouplers with field phototransistors (OFPT) – fig.9
- Optocouplers with an air gap (OAG) – fig.10
- Reflective optocouplers (RO) – fig.11

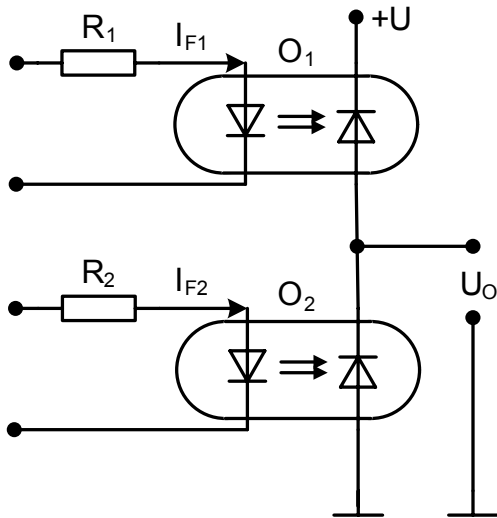


Fig. 6

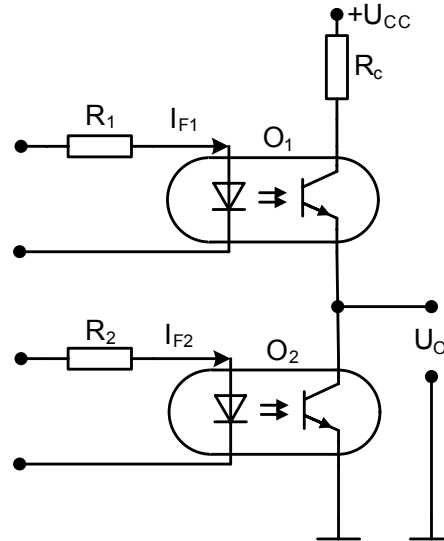


Fig. 7

When  $I_{F1} = 0$   $I_{F2} = 0$  and there is a symmetry in the circuit, the output voltage is:

$$(10) \quad U_o \approx \frac{1}{2} U_{CC}$$

Let's look at the PPO in fig.7:  $U_{CC} = 12 \text{ V}$

$$I_{F1} = 0 \quad I_{F2} = \max \quad U_o \min = U_{CEsat2} = 0,1 \text{ V}$$

$$I_{F1} = \max \quad I_{F2} = 0 \quad U_o \max = U_{CC} - U_{CEsat1} = 12 - 0,1 = 11,9 \text{ V}$$

The change range of the output voltage is:

$$(11) \quad D_U = \frac{U_o \max}{U_o \min} = \frac{U_{CC} - U_{CEsat1}}{U_{CEsat2}} = \frac{U_{CC} - 0,1}{0,1} = \frac{12 - 0,1}{0,1} = 119 (> 10^2)$$

The change range of the current is:

$$I_{F1} = 0, I_{F2} = 0, I_{D1} \approx I_{D2} = I_D, \text{ let } I_D = 100 \cdot 10^{-9} \text{ A (25}^\circ \text{ C) when } R_C = 10 \text{ k}\Omega$$

$$U_{CC} = 12 \text{ V}$$

$$(12) \quad I_C = \frac{U_{CC} - U_{CEsat1} - U_{CEsat2}}{R_C} = \frac{12 - 0,1 - 0,1}{10 \text{ k}\Omega} = 1,18 \text{ mA}$$

$$(13) \quad D_I = \frac{I_C}{I_D} = \frac{1,18 \cdot 10^{-3}}{100 \cdot 10^{-9}} = 1,18 \cdot 10^3 (> 10^3)$$

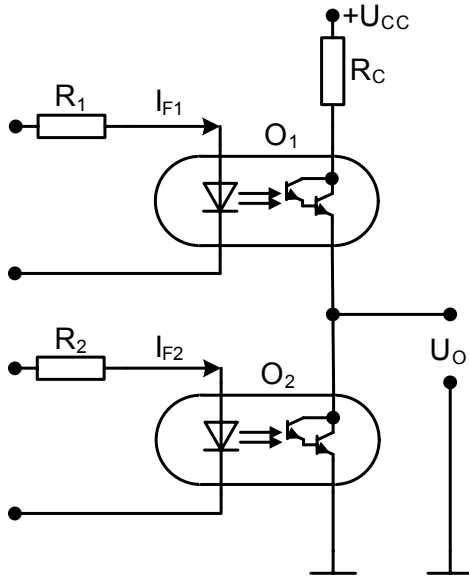


Fig. 8

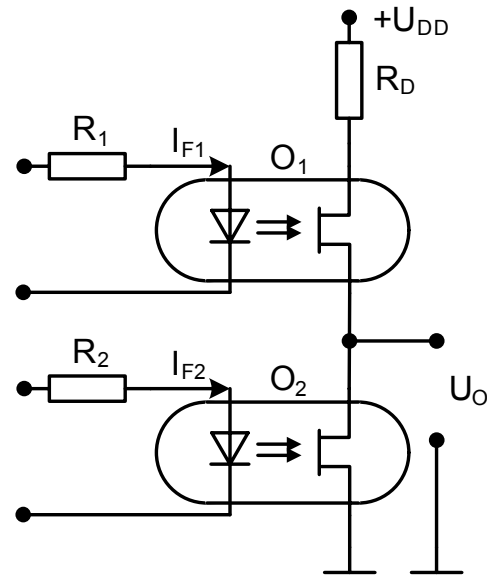


Fig. 9

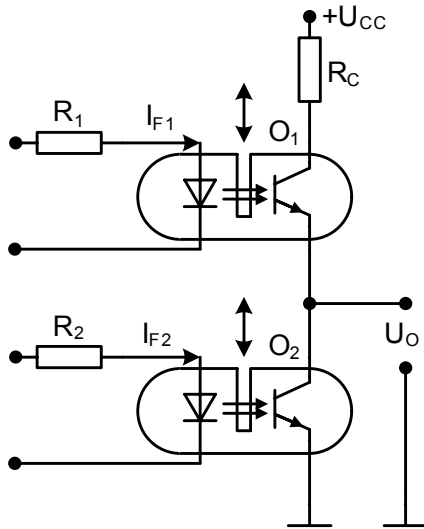


Fig. 10

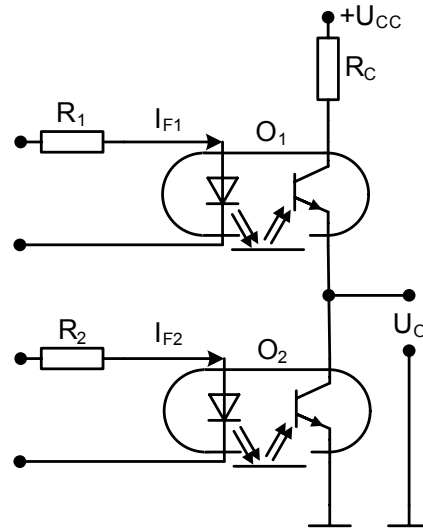


Fig. 11

The change range of the resistance collector/emitter  $R_{CE}$  of the phototransistor is:

$$(14) \quad R_{CEH} = \frac{0,5U_{CC}}{I_D} = \frac{6V}{100 \cdot 10^{-9}} = 600k\Omega$$

$$(15) \quad R_{CEL} = \frac{U_{CEsat}}{I_C} = \frac{0,1V}{1mA} = 100\Omega$$

$$(16) \quad D_{R_{CE}} = \frac{R_{CEH}}{R_{CEL}} = \frac{600 \cdot 10^3}{100} = 6 \cdot 10^3$$

### 5. GRAPHIC ANALYTICAL WAY OF CALCULATING OF PPO

A graphic-analytical way of calculating a PPO with phototransistor optocouplers (PTOs) is proposed:

1. From the transfer characteristic of the PTO:  
 $I_{ph}(I_C) = f(I_F) \quad U_{CE} = \text{const} \quad I_{FX} \longrightarrow I_{phx}$
2. From the input characteristic of the PDO:  
 $I_{ph} = f(U_{CE}); I_F = \text{const} \quad I_F, I_{phx} \longrightarrow U_{CEX}$
3.  $R_{CEX} = \frac{U_{CEX}}{I_{phx}}$
4. Building the dependence  $R_{CE} = f(I_F)$  (non-linear)  
 For photodiode optocouplers (PDOs):
  1. From the transfer characteristic of the PDO:  
 $I_{ph} = f(I_{FX}) \quad U = \text{const} \quad I_{FX} \longrightarrow I_{phx}$
  2. From the output characteristic:  
 $I_{ph} = f(I_F) \quad I_{phx}, I_{FX} \longrightarrow U_{AKX}$
  3.  $R_{AKX} = \frac{U_{AKX}}{I_{phx}}$
  4. Building the dependence  $R_{AKX} = f(I_F)$

Comparison of the PPO with different types of optocouplers – table 1:

Table 1

PPO type	Non-linearity, %	Change range	Basic changeable parameter	Frequency band, kHz
PRO	5 ÷ 10	< 10 <sup>6</sup>	resistance	10
PDO	1 ÷ 5	< 10 <sup>4</sup>	current	1 000
PTO	15	< 10 <sup>6</sup>	current	100
DPTO	20	< 10 <sup>6</sup>	current	30
OFPT	1 – (low )	< 10 <sup>6</sup>	resistance	80

The PPOs proposed can have more than 2 channels (3-8).

## 6. CONCLUSION

Contactless circuits of controllable photopotentiometric optocouplers – mono and stereo have been proposed, as well as analytical and graphic methods for calculating the photopotentiometric optocouplers. A comparison of PPOs according to the optocoupler type has been made.

## 7. REFERENCES

- [1]. Kolev, I.S. Infrared Optoelectronics. Gabrovo, University Publishing House “V. Aprilov”, 2004.
- [2]. Kolev, I.S. Optoelectronics. Gabrovo, University Publishing House “V. Aprilov”, 2004.
- [3]. Носов, Ю. Р. Оптоэлектроника. М., Радио и связь, 1989.
- [4]. Siemens. Optoelectronics. Data Book. 1993.
- [5]. Texas Instruments. Intelligent Opto Sensor, 1999.