

# A MOS Controlled Thyristor Model for PSpice Simulation

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**Abstract** - A PSpice model for the MOS controlled thyristor (MCT) consisting of a thyristor section and two MOSFET sections is proposed. The parameters of the equivalent circuit can be calculated from the data provided by the manufacturer and some simple measurements. The simulation results of a phase controlled rectifier show quite accurate behaviour of the proposed model.

**Keywords** - PSpice, simulation, modeling, MOS controlled thyristor, power semiconductor

## 1 INTRODUCTION

The MOS Controlled Thyristor (MCT) is a new power semiconductor device having several advantages compared with other devices. The MCT has a main thyristor section, and a gate control section for turning it on and off. Since the integration of the MCT is complex, it is very difficult to obtain an exact circuit model for the device. A complex model of the MCT has been developed by Harris Semiconductor [1]. A simpler model for the MCT would help to keep the simulation time and effort minimal. Such a model has been proposed in [2], but it seems that it does not simulate all the MCT characteristics properly (such as: SCR breakdown and breakover, turn-on spike voltages...).

This paper presents a simple circuit model for the P-type MCT suitable for analysis of MCT power converters. The model represents the characteristics of the MCT during turn-on and turn-off, as well as the breakdown and breakover characteristics of the SCR section, including their temperature dependence. The model parameters can be obtained from the specifications contained in the manufacturer's data sheet as described in [2], [3] and [4]. Extensive simulations have been performed in order to test the proposed model characteristics. The model has passed all performed tests and can be used to analyze various types of MCT power converters. The simulation results of an MCT phase-controlled rectifier are shown below.

## 2 CIRCUIT MODEL FOR THE MCT.

The PSpice model for the MCT is derived from the transistor level equivalent of MCT shown in Fig. 1. Its SCR section is developed by expanding the thyristor model presented in [3] and [4]. The gate control section consisting of a PMOS and an NMOS is modeled using simple RC circuits for the controlling of the turn-on and turn-off times and with simple diodes ( $D_{PMOS}$  and  $D_{NMOS}$ ) to isolate the operation of the MOSFET's in such a manner that the triggering pulse of one polarity activates only one FET.

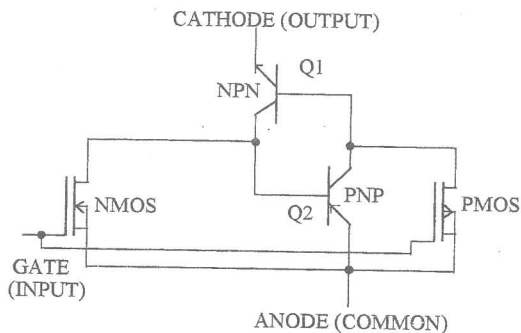


Fig. 1 Transistor level equivalent circuit of the MCT

The complete PSpice model is shown in Fig. 2 and the complete list of the PSpice statements for the subcircuit description of the proposed MCT model is presented in the appendix.

When a negative pulse is applied to the gate of the PMOS, the capacitor  $C_{PMOS}$  charges up. The voltage across  $C_{PMOS}$  increases the value of  $G_p$  which charges the capacitor  $C_p$ . The current through  $V_{GD}$  causes the positive current from  $F_{CTRL}$  and a negative voltage  $V(3,20)$  appears between nodes 3 and 20. The voltage across  $E_3$  will be zero and, as a consequence, the voltage across  $E_1$  will be also zero. The MCT is in conducting state. Once the MCT is turned on, the current through  $V_5$  will keep the device in the on state.

Once a positive pulse is applied to the gate, the capacitor  $C_{NMOS}$  charges, the  $G_p$  reverses its direction and so does the current from  $F_{CTRL}$ . The voltage across  $E_3$  rises to 1 and the voltage across  $E_1$  takes the value of the anode to cathode voltage. The MCT is in the off state. The behaviour of the SCR section of the model is explained in [3] and [4].

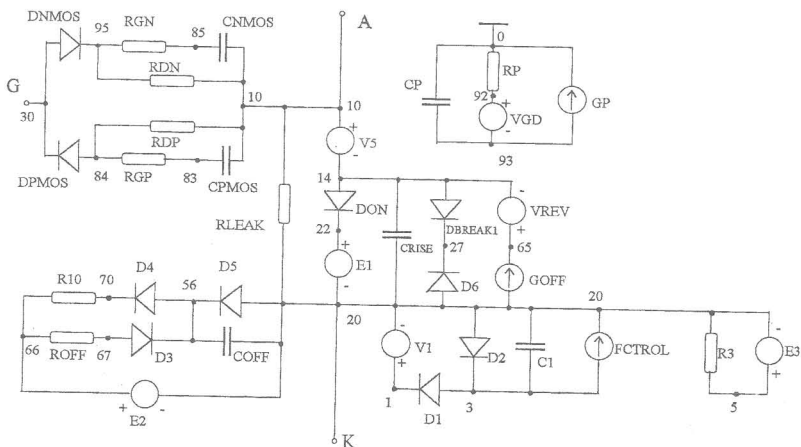


Fig. 2 PSpice model of the MCT

### 3 SIMULATION RESULTS

Extensive simulations have been performed in order to test the proposed model characteristics. The model has passed all performed tests and can be used to analyze various types of MCT power converters. The simulation results for the complete circuit of an MCT phase-controlled rectifier, shown in Fig. 3, are presented below. The converter uses a diode bridge to rectify the input ac voltage. The MCT is used as a phase-controlled switch to control the flow of power from the ac source. The diode  $D_m$  provides the freewheeling action. The waveforms of the input voltage, load voltage and gate pulses are shown in Fig. 4. Comparing them with the experimental waveforms shown in [2] it can be seen that the simulated waveforms agree very well with the experimental ones.

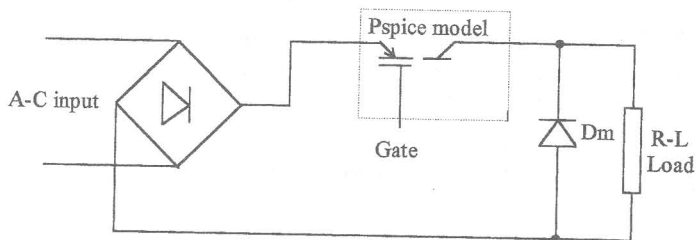


Fig. 3 Power circuit of the MCT phase-controlled rectifier

Date/Time run: 07/10/96 22:25:54

Temperature: 150.0

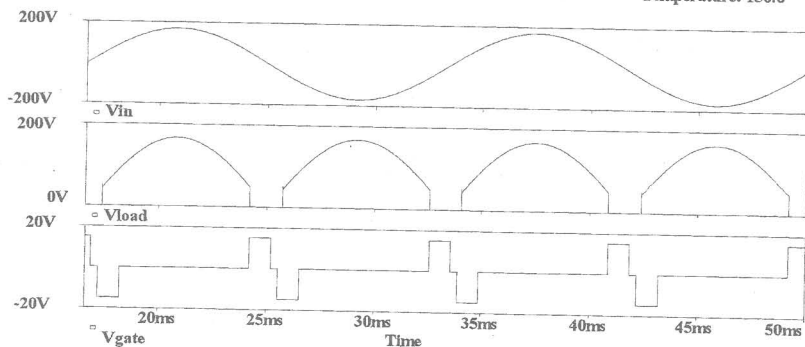


Fig. 4 Simulated MCT converter waveforms

#### 4 CONCLUSION

The paper presents a PSpice model of the MCT. The model has a thyristor section and two MOSFET sections for turning the MCT on and off. The model is simple and it represents the characteristics of the MCT during turn-on and turn-off, as well as the breakdown and breakover characteristics of the SCR section, including their temperature dependence. The extensive simulations performed show very good behaviour of the proposed model.

#### REFERENCES:

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## APPENDIX

### Subcircuit description of the MCT

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\*PSPICE MODEL FOR MCT

.SUBCKT MCT 10 20 30

\*-----A K G

\*PNPN STRUCTURE

.MODEL DMOD D

.MODEL DON1 D (RS=.019 IS=1E-12)

.MODEL DGAT D (IS=1E-12)

.MODEL DBREAK D (BV=900 IS=1E-7 XTI=3)

.MODEL DBREAK1 D (BV=20 IS=1E-7 XTI=3)

V1 1 20 DC .999

V5 10 14 DC 0

VREV 65 14 DC 0

D1 3 1 DMOD

D2 20 3 DMOD

D3 67 56 DMOD

D4 56 70 DMOD

D5 20 56 DMOD

DON 14 22 DON1

DBREAK 14 27 DBREAK1

D6 20 27 DBREAK

E1 22 20 POLY(2) 10 20 5 20 0 0 0 0 1

E2 66 20 10 20 -1

C1 3 20 .5UF IC=1.5

CRISE 14 20 INF

COFF 56 20 10NF

RLEAK 10 20 40K

ROFF 66 67 2.5

R10 66 70 1

G0FF 20 65 66 67 1

FCTROL 3 20 POLY (3) VGD V5 VREV -.1 1 .5 1

E3 5 20 TABLE {V(3,20)}=(.01V,0V) (1.25V,1V)

R3 5 20 10MEG

\*MOS STRUCTURE

RGP 83 84 5

RGN 85 95 5

CPMOS 10 83 18.92N

DPMOS 84 30 DPN

CNMOS 85 10 31.54N

DNMOS 30 95 DPN

RDP 10 84 100

RDN 10 95 100

.MODEL DPN D

GP 93 0 POLY(2) 10 83 10 85 0 6.423 32.15

RP 0 92 1

VGD 92 93 0

CP 0 93 .07U

.ENDS